

Levi-Civita formulation

2D system: u_1, u_2

$$\begin{aligned} R_1 &= u_1^2 - u_2^2 \\ R_2 &= 2u_1u_2 \end{aligned}$$

Transformation

$$\mathbf{R} = \mathcal{L}(\mathbf{u})\mathbf{u}$$

Levi-Civita [1920] matrix

$$\mathcal{L}(\mathbf{u}) = \begin{bmatrix} u_1 & -u_2 \\ u_2 & u_1 \end{bmatrix} \quad \Rightarrow \quad R = u_1^2 + u_2^2$$

Definition $\dot{\mathbf{R}}^2 = \dot{\mathbf{R}}^T \cdot \dot{\mathbf{R}}$ with $\mathbf{R}' = 2\mathcal{L}(\mathbf{u})\mathbf{u}'$ and $\dot{R} = R'/R$

$$\dot{\mathbf{R}} = 2\mathcal{L}(\mathbf{u})\mathbf{u}'/R$$

$\dot{\mathbf{R}}^T = 2\mathbf{u}'\mathcal{L}^T(\mathbf{u})/R$ and $\mathcal{L}^T(\mathbf{u})\mathcal{L}(\mathbf{u}) = R\mathbf{I}$ give

$$\dot{\mathbf{R}}^T \cdot \dot{\mathbf{R}} = 4\mathbf{u}' \cdot \mathbf{u}'/R$$

Final equation of motion, with $\mathbf{u} \cdot \mathbf{u} = R$

$$\mathbf{u}'' = \frac{1}{2}h\mathbf{u} + \frac{1}{2}R\mathcal{L}^T(\mathbf{u})\mathbf{F}_{kl}$$

Binding energy per unit reduced mass

$$h = [(2\mathbf{u}' \cdot \mathbf{u}' - (m_k + m_l)]/R$$

Rate of change from $\dot{\mathbf{R}} \cdot \ddot{\mathbf{R}}$

$$\frac{d}{dt} \left[\frac{1}{2}\dot{\mathbf{R}}^2 - \frac{(m_k + m_l)}{R} \right] = \dot{\mathbf{R}} \cdot \mathbf{F}_{kl}$$

Conversion by $h' = \mathbf{R}' \cdot \mathbf{F}_{kl}$ and $\dot{\mathbf{R}}$

$$h' = 2\mathbf{u}' \cdot \mathcal{L}^T(\mathbf{u})\mathbf{F}_{kl}$$

KS formulation

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$$R_2 = 2u_1u_2$$

Transformation

$$\mathbf{R} = \mathcal{L}(\mathbf{u})\mathbf{u}$$

Levi-Civita [1920] matrix

$$\mathcal{L}(\mathbf{u}) = \begin{bmatrix} u_1 & -u_2 \\ u_2 & u_1 \end{bmatrix} \Rightarrow R = u_1^2 + u_2^2$$

Matrix properties (Stiefel & Scheifele 1970)

$$\mathcal{L}^T(\mathbf{u})\mathcal{L}(\mathbf{u}) = R\mathbf{I}$$

$$\mathcal{L}'(\mathbf{u}) = \mathcal{L}(\mathbf{u}')$$

$$\mathcal{L}(\mathbf{u})\mathbf{v} = \mathcal{L}(\mathbf{v})\mathbf{u}$$

$$\mathbf{u} \cdot \mathbf{u}\mathcal{L}(\mathbf{v})\mathbf{v} - 2\mathbf{u} \cdot \mathbf{v}\mathcal{L}(\mathbf{u})\mathbf{v} + \mathbf{v} \cdot \mathbf{v}\mathcal{L}(\mathbf{u})\mathbf{u} = 0$$

Second & third properties give

$$\mathbf{R}' = 2\mathcal{L}(\mathbf{u})\mathbf{u}'$$

From $\mathcal{L}'(\mathbf{u}) = \mathcal{L}(\mathbf{u}')$

$$\mathbf{R}'' = 2\mathcal{L}(\mathbf{u})\mathbf{u}'' + 2\mathcal{L}(\mathbf{u}')\mathbf{u}'$$

Substituting $\mathbf{R}, \mathbf{R}', R' = 2\mathbf{u}' \cdot \mathbf{u}$ and $n = 1$ in smoothed \mathbf{R}''

$$\begin{aligned} 2\mathbf{u} \cdot \mathbf{u}\mathcal{L}(\mathbf{u})\mathbf{u}'' &+ 2\mathbf{u} \cdot \mathbf{u}\mathcal{L}(\mathbf{u}')\mathbf{u}' - 4\mathbf{u} \cdot \mathbf{u}'\mathcal{L}(\mathbf{u})\mathbf{u}' + \\ &+ (m_k + m_l)\mathcal{L}(\mathbf{u})\mathbf{u} = (\mathbf{u} \cdot \mathbf{u})^3 \mathbf{F}_{kl} \end{aligned}$$

Simplification by fourth property

$$2\mathbf{u} \cdot \mathbf{u} \mathcal{L}(\mathbf{u}) \mathbf{u}'' - 2\mathbf{u}' \cdot \mathbf{u}' \mathcal{L}(\mathbf{u}) \mathbf{u} + (m_k + m_l) \mathcal{L}(\mathbf{u}) \mathbf{u} = (\mathbf{u} \cdot \mathbf{u})^3 \mathbf{F}_{kl}$$

Multiply by $\mathcal{L}^{-1}(\mathbf{u})$ and first property

$$\mathbf{u}'' + \{[(m_k + m_l) - 2\mathbf{u}' \cdot \mathbf{u}'] / 2\mathbf{u} \cdot \mathbf{u}\} \mathbf{u} = \frac{1}{2} \mathbf{u} \cdot \mathbf{u} \mathcal{L}^T(\mathbf{u}) \mathbf{F}_{kl}$$

Definition $\dot{\mathbf{R}}^2 = \dot{\mathbf{R}}^T \cdot \dot{\mathbf{R}}$ with \mathbf{R}' and $\dot{R} = R' / R$

$$\dot{\mathbf{R}} = 2\mathcal{L}(\mathbf{u}) \mathbf{u}' / R$$

$\dot{\mathbf{R}}^T = 2\mathbf{u}' \mathcal{L}^T(\mathbf{u}) / R$ and orthogonality condition

$$\dot{\mathbf{R}}^T \cdot \dot{\mathbf{R}} = 4\mathbf{u}' \cdot \mathbf{u}' / R$$

Final equation of motion, with $\mathbf{u} \cdot \mathbf{u} = R$

$$\mathbf{u}'' = \frac{1}{2} h \mathbf{u} + \frac{1}{2} R \mathcal{L}^T(\mathbf{u}) \mathbf{F}_{kl}$$

Binding energy per unit reduced mass

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Rate of change from $\dot{\mathbf{R}} \cdot \ddot{\mathbf{R}}$

$$\frac{d}{dt} \left[\frac{1}{2} \dot{\mathbf{R}}^2 - \frac{(m_k + m_l)}{R} \right] = \dot{\mathbf{R}} \cdot \mathbf{F}_{kl}$$

Conversion by $h' = \mathbf{R}' \cdot \mathbf{F}_{kl}$ and $\dot{\mathbf{R}}$

$$h' = 2\mathbf{u}' \cdot \mathcal{L}^T(\mathbf{u}) \mathbf{F}_{kl}$$

Generalized 4×4 matrix

$$\mathcal{L}(\mathbf{u}) = \begin{bmatrix} u_1 & -u_2 & -u_3 & u_4 \\ u_2 & u_1 & -u_4 & -u_3 \\ u_3 & u_4 & u_1 & u_2 \\ u_4 & -u_3 & u_2 & -u_1 \end{bmatrix}$$

Explicit components of \mathbf{R}

$$\begin{aligned} R_1 &= u_1^2 - u_2^2 - u_3^2 + u_4^2 \\ R_2 &= 2(u_1 u_2 - u_3 u_4) \\ R_3 &= 2(u_1 u_3 + u_2 u_4) \\ R_4 &= 0 \end{aligned}$$

Summing the squares and square root

$$R = u_1^2 + u_2^2 + u_3^2 + u_4^2$$

Case $R_1 > 0$: combine R_1 and R

$$u_1^2 + u_4^2 = \frac{1}{2}(R_1 + R)$$

Redundancy $u_4 = 0$

$$\begin{aligned} u_1 &= \left[\frac{1}{2}(R_1 + R) \right]^{1/2} \\ u_2 &= \frac{1}{2} R_2 / u_1 \\ u_3 &= \frac{1}{2} R_3 / u_1 \end{aligned}$$

Case $R_1 < 0$: subtract R_1 from R

$$u_2^2 + u_3^2 = \frac{1}{2}(R - R_1)$$

Redundancy $u_3 = 0$

$$\begin{aligned} u_2 &= [\frac{1}{2}(R - R_1)]^{1/2} \\ u_1 &= \frac{1}{2}R_2/u_2 \\ u_4 &= \frac{1}{2}R_3/u_2 \end{aligned}$$

Regularized velocity: invert \mathbf{R}' and use first property

$$\mathbf{u}' = \frac{1}{2}\mathcal{L}^T(\mathbf{u})\mathbf{R}'/R = \frac{1}{2}\mathcal{L}^T(\mathbf{u})\dot{\mathbf{R}}$$

Final equations of motion

$$\begin{aligned} \mathbf{u}'' &= \frac{1}{2}h\mathbf{u} + \frac{1}{2}R\mathcal{L}^T\mathbf{F}_{kl} \\ h' &= 2\mathbf{u}' \cdot \mathcal{L}^T\mathbf{F}_{kl} \\ t' &= \mathbf{u} \cdot \mathbf{u} \end{aligned}$$

Semi-major axis

$$a = -\frac{1}{2}(m_k + m_l)/h$$

Eccentricity: $R = a(1 - e \cos \theta)$ and $nt = \theta - e \sin \theta$

$$e^2 = (1 - R/a)^2 + 4(\mathbf{u} \cdot \mathbf{u}')^2/[(m_k + m_l)a]$$

Bilinear relation: $\dot{R}_4 = 0$

$$u_4u'_1 - u_3u'_2 + u_2u'_3 - u_1u'_4 = 0$$

Unperturbed two-body motion

Maximum force:

$$j = \max_i (m_i/|\mathbf{r}_i - \mathbf{r}_{cm}|^2), \quad i = 1, N$$

Smallest inverse travel time

$$\beta_s = \mathbf{r}_s \cdot \dot{\mathbf{r}}_s / r_s^2, \quad \mathbf{r}_s - \mathbf{r}_{cm} \Rightarrow \mathbf{r}_s$$

Perturber boundary

$$r_\gamma = R[2\tilde{m}/(m_b\gamma_{\min})]^{1/3}$$

Travel time: $\dot{r}_s < 0$

$$\Delta t_{\text{in}} = (r_s - r_\gamma)/|\dot{r}_s|,$$

Free-fall time

$$\Delta t_a = [2\Delta t_{\text{in}}\dot{r}_s r_s^2/(m_b + m_s)]^{1/2}$$

Return time of dominant body

$$\Delta t_j = [2(r_j - r_\gamma)r_j^2/(m_b + m_j)]^{1/2}$$

Unperturbed time interval

$$\Delta t_\gamma = \min(\Delta t_{\text{in}}, \Delta t_a, \Delta t_j, \Delta t_{cm})$$

Unperturbed periods

$$K = 1 + \frac{1}{2}\Delta t_\gamma/t_K$$

Final time interval

$$\Delta t = K \min(t_K, \Delta t_{\text{cm}})$$

KS algorithms

Perturber prediction

$$\begin{aligned}\mathbf{r}_j &= \left(\left(\frac{1}{6} \mathbf{F}^{(1)} \delta t'_j + \frac{1}{2} \mathbf{F} \right) \delta t'_j + \mathbf{v}_0 \right) \delta t'_j + \mathbf{r}_0 \\ \dot{\mathbf{r}}_j &= \left(\left(\frac{1}{2} \mathbf{F}^{(1)} \delta t'_j + \mathbf{F} \right) \delta t'_j + \mathbf{v}_0 \right), \quad \delta t'_j = t - t_j\end{aligned}$$

KS prediction

\mathbf{u} and \mathbf{u}' to order $\mathbf{u}^{(5)}$

Basic Hermite

Stabilization factor in \mathbf{u}''

h predicted to order $h^{(2)}$

KS transformations

Global coordinates and velocities $\mathbf{r}_k, \mathbf{r}_l, \dot{\mathbf{r}}_k, \dot{\mathbf{r}}_l$

Physical perturbation

\mathbf{P} and $\dot{\mathbf{P}}$ due to perturbers, set $\mathbf{P}' = R \dot{\mathbf{P}}$

$j > N$: c.m. approximation or components

Slow-down factor

Include κ in \mathbf{P} and $\dot{\mathbf{P}}$, also $t' = \kappa \mathbf{u} \cdot \mathbf{u}$

Energy prediction (Stumpff method)

h to order $h^{(4)}$

KS corrector

\mathbf{u}, \mathbf{u}' to order $\mathbf{u}^{(5)}$ and h to $h^{(4)}$

Time derivatives

Taylor series $t'' = 2\mathbf{u} \cdot \mathbf{u}', \dots, t^{(6)} = 2\mathbf{u} \cdot \mathbf{u}^{(5)} + \dots$

Hermite KS

Standard KS

$$\begin{aligned}\mathbf{u}'' &= \frac{1}{2}h \mathbf{u} + \frac{1}{2}R \mathcal{L}^T \mathbf{F}_{kl} \\ h' &= 2 \mathbf{u}' \cdot \mathcal{L}^T \mathbf{F}_{kl} \\ t' &= \mathbf{u} \cdot \mathbf{u}\end{aligned}$$

New notation

$$\begin{aligned}\mathbf{F}_u &= \mathbf{u}'' \\ \mathbf{Q} &= \mathcal{L}^T \mathbf{P},\end{aligned}$$

with $\mathbf{P} = \mathbf{F}_{kl}$ as the perturbing force.

Basic equations

$$\begin{aligned}\mathbf{F}_u &= \frac{1}{2}h \mathbf{u} + \frac{1}{2}R \mathbf{Q} \\ h' &= 2 \mathbf{u}' \cdot \mathbf{Q} \\ t' &= \mathbf{u} \cdot \mathbf{u}\end{aligned}$$

Hermite \mathbf{F} , \mathbf{F}' formulation

$$\begin{aligned}\mathbf{F}_u &= \frac{1}{2}h \mathbf{u} + \frac{1}{2}R \mathbf{Q} \\ \mathbf{F}'_u &= \frac{1}{2}(h' \mathbf{u} + h \mathbf{u}' + R' \mathbf{Q} + R \mathbf{Q}') \\ h' &= 2 \mathbf{u}' \cdot \mathbf{Q} \\ h'' &= 2 \mathbf{F}_u \cdot \mathbf{Q} + 2 \mathbf{u}' \cdot \mathbf{Q}' \\ t' &= \mathbf{u} \cdot \mathbf{u}\end{aligned}$$

The derivatives of \mathbf{P} , \mathbf{Q} and t' are readily available. Note that $\mathbf{P}' = R\dot{\mathbf{P}}$ and that $\mathcal{L}^T(\mathbf{u}')$ can be obtained by substituting \mathbf{u}' for \mathbf{u} . For implementation, significant accuracy can be gained by high-order prediction (not used in standard Hermite).

N-body interface

Centre of mass acceleration

$$\ddot{\mathbf{r}}_{cm} = (m_k \mathbf{F}_k + m_l \mathbf{F}_l) / (m_k + m_l)$$

Global coordinates

$$\begin{aligned}\mathbf{r}_k &= \mathbf{r}_{cm} + \mu \mathbf{R} / m_k \\ \mathbf{r}_l &= \mathbf{r}_{cm} - \mu \mathbf{R} / m_l\end{aligned}$$

Relative perturbation

$$\gamma = |\mathbf{F}_k - \mathbf{F}_l| R^2 / (m_k + m_l)$$

Tidal approximation

$$r_\gamma = R[2\tilde{m}/(m_k + m_l)\gamma_{\min}]^{1/3}, \quad \gamma_{\min} \simeq 10^{-6}$$

Perturber selection

$$r_{ij} < r_\gamma, \quad R = a(1 + e)$$

Regularized time-step

$$\Delta\tau = \eta_u (1/2|h|)^{1/2} 1/(1 + 1000\gamma)^{1/3}$$

Physical time-step

$$\Delta t = \sum_{k=1}^n \frac{1}{k!} t_0^{(k)} \Delta\tau^k, \quad n = 6$$

Time derivatives

$$\begin{aligned}t_0'' &= 2\mathbf{u}' \cdot \mathbf{u} \\ t_0^{(3)} &= 2\mathbf{u}'' \cdot \mathbf{u} + 2\mathbf{u}' \cdot \mathbf{u}\end{aligned}$$